



## Editor's choice paper

# Properties of alkali-promoted Cu–MgO catalysts and their activity for methanol decomposition and C<sub>2</sub>-oxygenate formation

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## ABSTRACT

The decomposition of CH<sub>3</sub>OH in the presence of CO has been investigated over high surface area MgO, Cu–MgO, K–Cu–MgO and Cs–Cu–MgO catalysts. The catalysts were prepared by thermal decomposition of metal salts mixed with palmitic acid. The reduced catalysts had surface areas of 18–74 m<sup>2</sup> g<sup>-1</sup> and intrinsic basicities of 4–17 μmol CO<sub>2</sub> m<sup>-2</sup>. Results revealed that methyl formate was a primary product of CH<sub>3</sub>OH decomposition, whereas CO was a secondary product. Although selectivity to C<sub>2</sub> species (ethanol and acetic acid) was low (<5 C-atom %) at the low pressure (101 kPa) conditions of the present study, there was an optimum intrinsic basicity (9.5 μmol CO<sub>2</sub> m<sup>-2</sup>) at which the selectivity to C<sub>2</sub> species and methyl formate reached a maximum. The role of catalyst basic properties in the formation of C<sub>2</sub> species from CH<sub>3</sub>OH is discussed.

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## 1. Introduction

Current interest in the production and use of oxygenate fuels stems in part from a concern for the environmental impact of fossil fuels used in the transportation sector. A major concern in this regard, is the emission of NO<sub>x</sub> and other toxic, ozone depleting chemicals from automobile exhausts. Attempts to reduce these emissions include the use of reformulated gasolines that in the past have contained small amounts of methyl tertiary butyl ether (MTBE). As MTBE is phased out and ethanol is seen as a potential alternative, there is an increased interest in new synthesis routes to ethanol. Although most of the world's ethanol is produced by fermentation, the process is expensive and energy inefficient due to intensive distillation steps [1,2]. An alternative approach, which also has significant potential to reduce greenhouse gas emissions associated with fossil fuels, is the selective conversion of biomass-derived syngas (CO/CO<sub>2</sub>/H<sub>2</sub>) to ethanol.

The low-temperature methanol synthesis from syngas, operated at 5–10 MPa and 473–573 K, is one of the most selective industrial processes carried out on a commodity scale [3–10]. During the last two decades, there has been significant research on the devel-

opment of catalysts that shift the synthesis away from methanol and towards higher alcohols, especially C<sub>2</sub>–C<sub>4</sub> alcohols [11–22]. Promotion of Cu–ZnO–Al<sub>2</sub>O<sub>3</sub> low-temperature methanol synthesis catalysts with alkali metals, increases the higher alcohol yield and selectivity [14,20,22,23]. However, these catalysts produce mostly isobutanol with a low selectivity to ethanol. Mechanistic studies have shown that over these catalysts, the first C–C coupling step occurs over basic sites [14,24–28,31]. In addition, methyl formate has been identified as an important intermediate species for ethanol synthesis from syngas and methanol [14,27], the yield of which is enhanced by alkali promotion of Cu–ZnO [14]. It has also been shown that Cu plays an important role in methanol dehydrocoupling to methyl formate [29,30]. These mechanistic studies suggest that catalysts with higher basicity than alkali-promoted Cu–ZnO catalysts could potentially enhance the rate of the first C–C coupling step in alcohol synthesis and thereby increase selectivity to ethanol. Several studies have reported on the basicity of alkali promoted MgO [32–35], demonstrating that alkali promoted MgO possesses high basicity. For example, the basic site density of MgO has been reported as 2.2–7.2 μmol CO<sub>2</sub> m<sup>-2</sup> [32–35] whereas for ZnO–ZrO<sub>2</sub> a value of 0.9 μmol CO<sub>2</sub> m<sup>-2</sup> has been reported [36].

Noting the above properties of Cu, MgO, alkali promoters and the proposed mechanism of the first C–C bond formation step in alcohol synthesis from syngas, the present work has focused on alkali-promoted Cu–MgO catalysts to better understand the effect of

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increased basicity on the mechanistic pathways to  $C_2$  species from  $C_1$  species ( $CH_3OH$  and  $CO$ ). In the first part of the study, the preparation and characterization of high surface area, alkali-promoted Cu–MgO catalysts is reported. Subsequently, the activity of these catalysts for methanol decomposition and C–C bond formation has been determined. The synthesis of alcohols from syngas is usually done at high pressures (>5 MPa) to overcome thermodynamic yield limitations of the methanol synthesis [14,20,22,23]. In the present work, however, low pressure (101 kPa) has been used to simplify the experimental procedures. Furthermore, by using  $CH_3OH$  as reactant and operating at low pressure, the decomposition of the feed  $CH_3OH$  that will generate surface species that can react further to produce  $C_2$  species, is assured. A related study of ethanol and higher alcohol formation from  $CH_3OH$  over a Cu–MgO– $Al_2O_3$  catalyst, reported recently, also used low pressure (101 kPa) [37]. Although no catalytic activity towards ethanol and higher alcohols was reported, dimethyl ether was produced.

In the present work, we report on the products generated from reactions of  $CH_3OH$  in the presence of  $CO$ ,  $H_2$  or  $He$ , at low pressure (101 kPa) as a function of the alkali-promoted Cu–MgO catalyst properties and use these data to provide insights into potential pathways for higher ethanol selectivity in syngas conversion. In future work, the same catalysts will be examined under high pressure conditions for syngas conversion.

## 2. Experimental

### 2.1. Catalyst preparation

High surface area, MgO, Cu–MgO, alkali-promoted Cu–MgO (0.5 wt% K–Cu–MgO, 4.4 wt% K–Cu–MgO, 0.5 wt% Cs–Cu–MgO and 13.5 wt% Cs–Cu–MgO) and bulk CuO were prepared by thermal decomposition of metal salts in the presence of palmitic acid ( $CH_3(CH_2)_{14}COOH$ ) [38]. Note that the 4.4 wt% K and the 13.5 wt% Cs promoted Cu–MgO catalysts had the same alkali/Mg molar ratio of 0.08.  $Mg(NO_3)_2 \cdot 6H_2O$ ,  $Cu(NO_3)_2 \cdot 3H_2O$ ,  $Cs_2CO_3$  and  $KNO_3$  were used as the source of MgO, Cu,  $Cs_2O$  and  $K_2O$ , respectively. The molar ratio of palmitic acid to [Mg + Cu + alkali metal] was 2.5 [38]. Note that in all cases the catalysts were nominally 40 wt% Cu and 60 wt% MgO when in the reduced state. As an example, to prepare the 0.5 wt% Cs–Cu–MgO catalyst, 6.00 g of  $Mg(NO_3)_2 \cdot 6H_2O$  (Sigma–Aldrich, 99%), 2.47 g of  $Cu(NO_3)_2 \cdot 3H_2O$  (AlfaAesar, 98–102%), 0.01 g  $Cs_2CO_3$  (Sigma–Aldrich, 99%) and 21.89 g palmitic acid (Sigma–Aldrich, 98%) were mechanically mixed in a crucible without adding water and placed in a furnace (Barnstead/Thermolyne 47900) in air at ambient pressure. The mixture was heated to 373 K for 60 min at  $40 K min^{-1}$  followed by heating to 445 K for 60 min at  $40 K min^{-1}$ . The solid catalyst precursor was obtained by subsequent calcination at 673 K. Calcination was achieved at a heat up rate of  $0.8 K min^{-1}$  and the final temperature was held for 300 min before cooling to room temperature. Finally, the catalyst precursor was reduced by heating to 573 K at a rate of  $10 K min^{-1}$  in 10%  $H_2/He$ , with the final temperature held for 60 min in 100%  $H_2$ , yielding 1.59 g of the 0.5 wt% Cs–Cu–MgO catalyst.

Note that the final calcination temperature used for each catalyst precursor was determined by the highest decomposition temperature of the metal nitrates or carbonates present in the precursor. For MgO, Cu–MgO, K–Cu–MgO and Cs–Cu–MgO the calcination temperatures were 673 K, 673 K, 873 K and 923 K, respectively. The effect of calcination temperature, calcination time and the amount of palmitic acid used in the preparation of the MgO was also examined. In addition, one sample of MgO was prepared without the use of palmitic acid and consequently, in this case, the thermal treatment prior to calcination that was conducted on the MgO-based catalysts (373 K for 60 min and 445 K for 60 min) was not necessary.

### 2.2. Catalyst characterization

Temperature-programmed reduction (TPR) of the prepared catalyst precursors was performed in a 10%  $H_2/Ar$  gas flow of  $50 cm^3(STP) min^{-1}$  and heating at a ramp rate of  $10 K min^{-1}$  from 313 K to 623 K, with the final temperature held for 30 min. Prior to the TPR, samples (about 0.2 g) were pre-treated thermally in  $He$  at  $50 cm^3(STP) min^{-1}$  and 393 K. Hydrogen consumption was monitored by a thermal conductivity detector (TCD) attached to a Micromeritics AutoChem II chemisorption analyzer. During the analysis the effluent gas was passed through a cold trap placed before the TCD in order to remove water from the exit stream of the reactor. Both CuO and  $Cu_2O$  (97% purity, particle size <5  $\mu m$ , Sigma–Aldrich) were also examined by TPR.

Catalyst BET surface areas were measured before and after reduction whereas the catalyst pore volume and pore diameter were measured before reduction only. The mentioned properties of the un-reduced catalysts were determined from  $N_2$  adsorption–desorption isotherms measured at 77 K using a Micromeritics ASAP 2020 analyzer. Catalysts were degassed in 523 K for 24 h under vacuum (5  $\mu m Hg$ ) before being analyzed. Eight  $N_2$  uptake measurements made in the range  $0.06 < P_{N_2}/P_{N_2}^0 < 0.20$  were used to calculate the BET surface area. The uptake of  $N_2$  at  $P_{N_2}/P_{N_2}^0 = 0.975$  was used to specify the catalyst pore volume. Pore diameter was calculated based on the pore size distribution measured from the  $N_2$  desorption in the range of  $0.01 < P_{N_2}/P_{N_2}^0 < 0.99$ .

The BET surface area of the reduced catalysts was measured using the Micromeritics AutoChem II chemisorption analyzer. The catalysts were first degassed in  $50 cm^3(STP) min^{-1}$   $He$  by heating from ambient temperature to 523 K and holding at 523 K for 120 min. The catalysts were then cooled to room temperature and the feed gas was switched from  $He$  to 10%  $H_2$  in  $Ar$  at a flow rate of  $50 cm^3(STP) min^{-1}$ . The TPR analysis described above was then conducted on the catalyst. Since MgO adsorbs  $CO_2$  and  $H_2O$ , pre-treatment in  $He$  at high temperature (773 K) was required [39–41] after reduction and prior to the surface area measurement. Hence the gas flow was switched from 10%  $H_2$  in  $Ar$  to  $He$  at a flow rate of  $50 cm^3(STP) min^{-1}$  and heated to 773 K at a rate of  $10 K min^{-1}$  for 60 min. The catalysts were then cooled to room temperature and the feed gas switched from  $He$  to 30 vol%  $N_2$  in  $He$  at a flow rate of  $50 cm^3(STP) min^{-1}$ . The single point BET surface area of the reduced catalyst was calculated by measuring the  $N_2$  uptake of the catalyst at 77 K using the liquid  $N_2$  trap.

Basic properties of the reduced catalysts were determined by  $CO_2$  temperature-programmed desorption (TPD) using a Micromeritics AutoChem II chemisorption analyzer. The reduced catalysts were pre-treated thermally by ramping to 773 K at  $10 K min^{-1}$  for 60 min in  $50 cm^3(STP) min^{-1}$  of  $He$ . After cooling to 313 K, the sample was exposed to  $50 cm^3(STP) min^{-1}$  of 10 vol%  $CO_2/He$  for 60 min. Physically adsorbed  $CO_2$  was subsequently removed from the sample by flushing in  $He$  ( $50 cm^3(STP) min^{-1}$ ) at 313 K for 60 min. The catalyst's basic properties were evaluated by observing the capacity of the samples to retain the  $CO_2$  during the desorption that occurred in the  $He$  flow while increasing temperature from 313 K to 803 K at a rate of  $10 K min^{-1}$ . The obtained  $CO_2$  TPD profile was integrated to determine the catalyst intrinsic basicity, defined as the total  $CO_2$  uptake divided by the BET surface area, and taken as a measure of the catalyst basic site density. To quantify the strength of the basic sites, the  $CO_2$  TPD profiles were de-convoluted to classify weak (353–373 K), medium (373–473 K) and strong (>473 K) basic sites according to their temperature of desorption.

X-ray powder diffraction (XRD) patterns of the prepared catalysts were obtained with a Rigaku Multiflex diffractometer using Cu  $K\alpha$  radiation ( $\lambda = 0.154 nm$ , 40 kV and 20 mA), a scan range of  $2\theta$

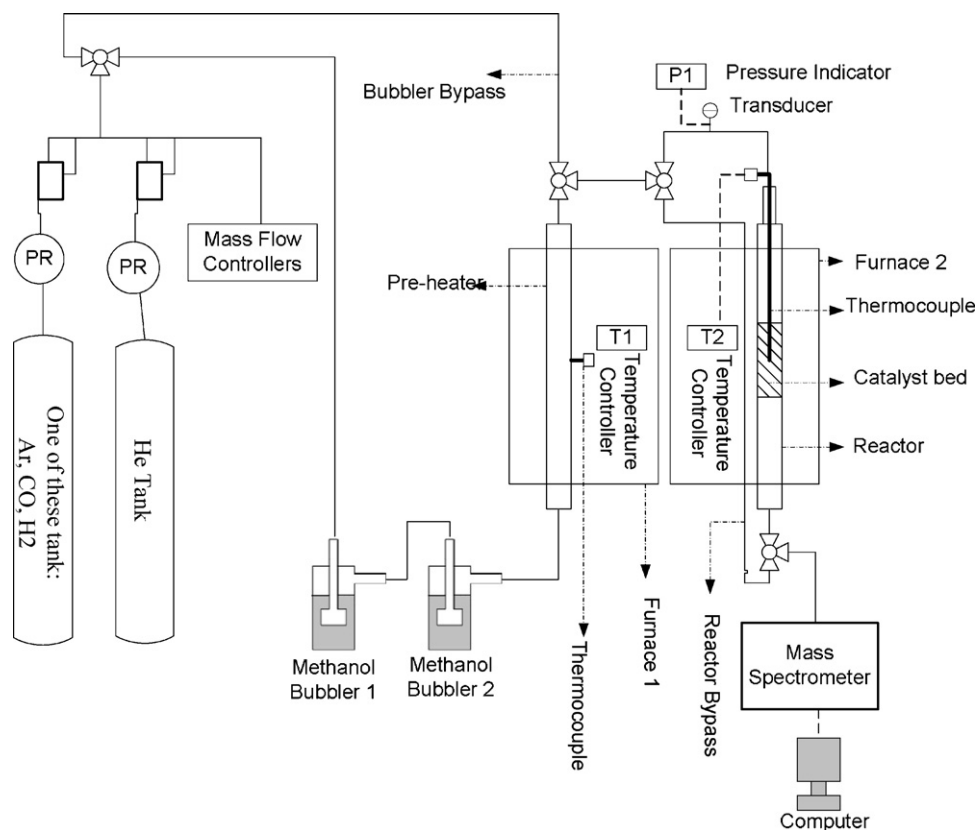


Fig. 1. Schematic diagram of the reactor setup.

from  $10^\circ$  to  $100^\circ$  and a step size of  $2^\circ$  per min. Crystallite size of the metal or metal oxide was estimated from the XRD data using the Scherrer equation. The Cu crystallite thickness ( $d_{\text{Cu}}^{\text{XRD}}$ ) was estimated from the CuO crystallite size ( $d_{\text{CuO}}^{\text{XRD}}$ ) determined from the XRD data of the non-reduced MgO-based catalysts, and the peak broadening at  $2\theta = 35.5^\circ$ . The Cu crystallite size was then estimated as:  $d_{\text{Cu}}^{\text{XRD}} = (\text{Cu molar volume}/\text{CuO molar volume}) \times d_{\text{CuO}}^{\text{XRD}}$ . The MgO crystallite size ( $d_{\text{MgO}}^{\text{XRD}}$ ) was measured based on the peak broadening at  $2\theta = 42.9^\circ$ .

The Cu dispersion of the reduced catalysts was measured by adsorption and decomposition of  $\text{N}_2\text{O}$  on the surface of Cu according to the stoichiometry:  $2\text{Cu}^0 + \text{N}_2\text{O} \rightarrow \text{N}_2 + \text{Cu}_2\text{O}$ . The pulse titration technique was used. Following reduction, the catalysts were pre-treated thermally by heating to 773 K at a rate of  $10 \text{ K min}^{-1}$  for 60 min in a flow of  $50 \text{ cm}^3(\text{STP}) \text{ min}^{-1}$  of He. The catalysts were then cooled to room temperature before the  $\text{N}_2\text{O}$  pulse titration was initiated using 10%  $\text{N}_2\text{O}/\text{N}_2$  as the pulse gas. A TCD attached to a Micromeritics AutoChem II chemisorption analyzer was used to detect the consumption of  $\text{N}_2\text{O}$  and Cu dispersion was calculated from the total amount of  $\text{N}_2\text{O}$  consumed. A liquid Ar trap was used to condense  $\text{N}_2\text{O}$  from  $\text{N}_2$  in the effluent, and hence only the  $\text{N}_2$  was detected by the TCD.

### 2.3. Catalyst testing

Catalyst testing was conducted in a stainless steel fixed bed tubular reactor shown in Fig. 1, operated at atmospheric pressure with inert He and Ar mixed with CO,  $\text{H}_2$  and  $\text{CH}_3\text{OH}$  as reactants. The catalyst (0.1–1.98 g) was loaded into the isothermal section of the reactor and reduced in 10%  $\text{H}_2/\text{He}$  at a flow rate of  $100 \text{ cm}^3(\text{STP}) \text{ min}^{-1}$  and a ramp rate of  $10 \text{ K min}^{-1}$  from ambient temperature to 573 K. After further heating in pure He to 773 K, the reactor was cooled to the desired reaction temperature. The desired reactant gases at a total flowrate of  $72 \text{ cm}^3(\text{STP}) \text{ min}^{-1}$  passed through two saturators in series containing pure  $\text{CH}_3\text{OH}$  at ambient temperature to generate the  $\text{CH}_3\text{OH}$  vapor ( $12 \text{ cm}^3(\text{STP}) \text{ min}^{-1}$ ). The feed mixture then passed through a pre-heater at 383 K before entering the reactor. The gas flow lines between the pre-heater and the reactor as well as between the reactor and the mass spectrometer were held at the same temperature as the pre-heater (383 K) using heating tapes. The reactor product composition was determined using a VG ProLab quadrupole mass spectrometer that continuously monitored the reactor exit gas line. In the present work, the focus was on the initial activity of the catalysts that were to be related to the properties of the fresh catalysts. Hence, after a 10 min reactor

Table 1

Effect of calcination temperature, calcination time and palmitic acid content on BET surface area, pore volume and pore size of MgO.

Catalyst	Calcination temperature (K)	Calcination time (min)	$R^a$ (-)	$S_{\text{BET}}^b$ ( $\text{m}^2 \text{ g}^{-1}$ )	$V_p^b$ ( $\text{cm}^3 \text{ g}^{-1}$ )	$d_p^b$ (nm)
MgO <sup>c</sup>	673	300	2.5	160	0.58	14.5
MgO-1	723	300	2.5	132	0.46	14.2
MgO-2	673	480	2.5	150	0.52	13.9
MgO-3	673	480	1.25	160	0.41	10.3
MgO-4	673	480	0.00	7	0.02	8.9

<sup>a</sup>  $R$  is molar ratio of palmitic acid to Mg + Cu + alkali metal.

<sup>b</sup>  $S_{\text{BET}}$ ,  $V_p$  and  $d_p$  are respectively, BET surface area, pore volume and average pore size of MgO catalyst before reduction.

<sup>c</sup> These conditions have been used for preparation of all Cu–MgO-based catalysts of the present study.

**Table 2**  
BET surface area, pore volume and pore size of alkali-promoted Cu–MgO catalysts.

Catalyst	Catalyst composition (A/Cu/MgO) <sup>a</sup> (wt%)	$S_{\text{BET}}^b$ ( $\text{m}^2 \text{g}^{-1}$ )		$V_p^b$ ( $\text{cm}^3 \text{g}^{-1}$ )	$d_p^b$ (nm)
		Before reduction	After reduction		
Cu–MgO	0/40.3/59.7	62	74	0.23	15.0
0.5 wt% K–Cu–MgO	0.5/40.1/59.3	35	42	0.20	23.1
0.5 wt% Cs–Cu–MgO	0.5/40.1/59.4	38	44	0.20	20.8
4.4 wt% K–Cu–MgO	4.4/38.2/56.5	26	30	0.17	26.4
13.5 wt% Cs–Cu–MgO	13.5/34.6/51.1	15	18	0.06	16.1

<sup>a</sup> A is alkali metal.

<sup>b</sup>  $S_{\text{BET}}$ ,  $V_p$  and  $d_p$  are respectively, BET surface area, pore volume and average pore size of MgO catalyst before reduction.

stabilization period, data were collected over the next 10 min and the average of these analyses are reported herein. Both diagnostic tests and calculation were used to confirm that at the chosen conditions, the catalyst activity data were free of both internal and external heat and mass transfer effects. For each experiment the performance of the catalyst was compared to an identical experiment conducted in the absence of the catalyst so that the effect of thermal reactions or activity from the wall of the reactor were accounted for. The data reported herein are net of the blank run conversions and product yields. In each experiment conversion was defined as the total C-atom conversion of  $\text{CH}_3\text{OH}$  or  $[\text{CH}_3\text{OH} + \text{CO}]$  in the case that CO was present in the feed. In most cases however, there was no net CO consumption since  $\text{CH}_3\text{OH}$  decomposed mostly to CO. The product yield was calculated as the product of the total exit molar flow rate and the component mole fraction. Component selectivity was determined as the total C-atom conversion divided by the product yield.

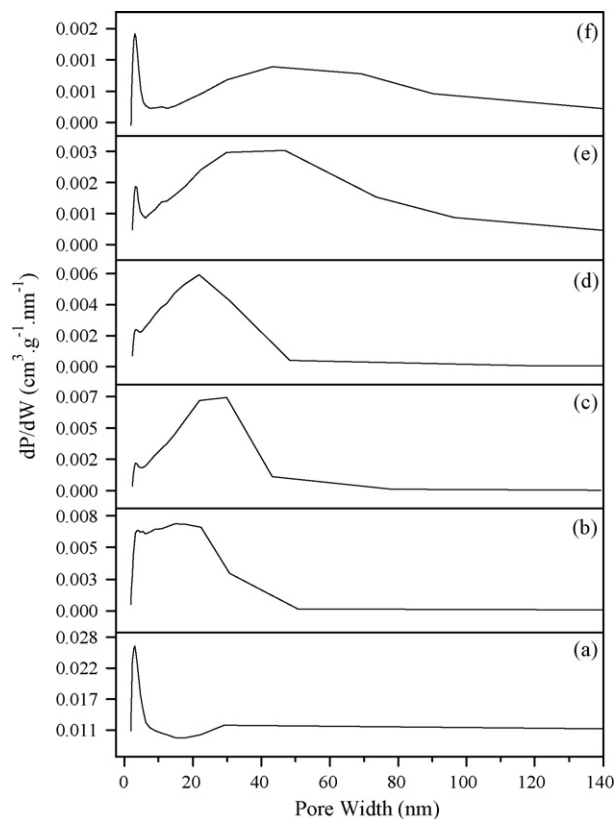
### 3. Results and discussion

#### 3.1. Catalyst characterization

The effect of preparation conditions on the properties of the MgO are reported in Table 1. Increased calcination temperature or calcination time decreased the BET surface area ( $S_{\text{BET}}$ ) and the pore volume ( $V_p$ ) of the MgO, most likely due to thermal sintering of the MgO crystallites. The  $S_{\text{BET}}$  results of Table 1 also show that a decrease in the mole fraction of palmitic acid used in the catalyst preparation led to an increase in the  $S_{\text{BET}}$  of the MgO. Following calcination, the MgO was grey in color, indicative of some carbonaceous residue from the palmitic acid not completely removed during calcination. With less palmitic acid, a lighter grey powder was produced, indicative of less carbonaceous impurity. The carbonaceous residue was likely responsible for the small decrease in surface area (through pore blockage) as the amount of palmitic acid increased. Note that the color of the MgO obtained from the thermal decomposition of  $\text{Mg}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  in the absence of palmitic acid was white (Table 1, MgO-4). Cosimo et al. [34] prepared MgO by thermal decomposition of  $\text{Mg}(\text{OH})_2$  in a high flow of air and reported an MgO surface area of  $119 \text{ m}^2 \text{ g}^{-1}$ , whereas the  $S_{\text{BET}}$  of MgO of the present study was  $160 \text{ m}^2 \text{ g}^{-1}$  (Table 1, MgO) and the thermal decomposition of  $\text{Mg}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  in the absence of palmitic acid (Table 1, MgO-4) yielded MgO with a  $S_{\text{BET}}$  of  $7 \text{ m}^2 \text{ g}^{-1}$ . These results show the advantage of using palmitic acid to obtain higher surface area MgO. Palmitic acid plays an important role by limiting the sintering of the MgO, likely due to the fact that palmitic acid is a good chelating agent for  $\text{Mg}^{2+}$ . The method used herein to obtain high surface area MgO is more convenient and simpler than conventional thermal decomposition methods, wherein high flows of purge gas are typically required to remove produced water and thereby limit sintering of the MgO [34].

The properties of the alkali-promoted Cu–MgO catalysts are reported in Table 2. Compared to the data of Table 1 for MgO,

the data show that addition of Cu to the MgO resulted in a loss of more than 50% of the MgO  $S_{\text{BET}}$  and  $V_p$ . The loss in  $S_{\text{BET}}$  and  $V_p$  could be partially due the fact that the CuO blocks the pores of the MgO, as suggested by others [42]. The pore size distributions of the MgO-based catalysts after calcination are shown in Fig. 2. The addition of the Cu to the MgO led to a significant increase in pore size, with the maxima of the pore size distribution occurring at much higher pore size compared to MgO (Fig. 2a, b). This supports the assertion that the smaller pores of the MgO were blocked by the CuO (before reduction). Nonetheless, the preparation method used herein yielded Cu–MgO with relatively high surface areas. For example, Nagaraja et al. [44] used co-precipitation to prepare Cu–MgO (nominally 40 wt% Cu and 60 wt% MgO) and reported a  $S_{\text{BET}}$  of  $28 \text{ m}^2 \text{ g}^{-1}$  [44], whereas in the present study the  $S_{\text{BET}}$  of the Cu–MgO was  $62 \text{ m}^2 \text{ g}^{-1}$  and  $74 \text{ m}^2 \text{ g}^{-1}$  before and after reduction, respectively. For all of the prepared catalysts of Table 2, the  $S_{\text{BET}}$  increased by about 20% after reduction, a result of the water loss associated with the reduction of CuO to Cu. The catalyst average pore size ( $d_p$ ) of the Cu–MgO catalysts, also reported in Table 2, shows that all of the prepared catalysts were mesoporous.



**Fig. 2.** Pore size distribution of un-reduced Cu–MgO-based catalysts: (a) MgO; (b) Cu–MgO; (c) 0.5 wt% K–Cu–MgO; (d) 0.5 wt% Cs–Cu–MgO; (e) 4.4 wt% K–Cu–MgO; (f) 13.5 wt% Cs–Cu–MgO.

Addition of Cs or K to the Cu–MgO also decreased the  $S_{\text{BET}}$  and  $V_p$ . Noting that the K promoted Cu–MgO and the Cs promoted Cu–MgO precursors were calcined at higher temperatures than the MgO and the Cu–MgO, it is likely that thermal sintering contributed to the decreased  $S_{\text{BET}}$  and  $V_p$  of the alkali-promoted Cu–MgO. Table 2 also shows that increasing the K loading of the K–Cu–MgO catalyst from 0.5 wt% to 4.4 wt%, decreased the catalyst  $S_{\text{BET}}$  and  $V_p$ . Similar effects were observed for the Cs promoted Cu–MgO catalyst as the Cs loading increased from 0.5 wt% to 13.5 wt%. Pore blockage of MgO by  $\text{Cs}_2\text{O}$  or  $\text{K}_2\text{O}$  has been reported in the literature [42] and the trends observed with increased promoter concentration suggest that similar effects are important here as well. The pore size distribution data of Fig. 2c, e show that increasing the K loading of the K promoted Cu–MgO catalyst from 0.5 wt% to 4.4 wt%, led to a significant increase in pore size with the maxima of the pore size distribution occurring at a higher pore size with increased K. The same trend was observed as the Cs loading of the Cs–Cu–MgO was increased from 0.5 wt% to 13.5 wt% (Fig. 2c, e). These observations support the assertion that the decreased  $S_{\text{BET}}$  of the K or Cs promoted Cu–MgO, compared to the Cu–MgO, was partially due to MgO pore blockage by  $\text{K}_2\text{O}$  or  $\text{Cs}_2\text{O}$ . Also, note that the melting point and boiling point of palmitic acid are 336 K and 623 K, respectively [43] whereas for  $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$  the melting point and boiling point are 387 K and 443 K, respectively [43]. Clearly both the  $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$  and the palmitic acid are mixed in the liquid phase below 443 K, the temperature to which the catalyst precursors were heated during preparation.  $\text{KNO}_3$  has a melting point and boiling point of 607 K and 673 K, respectively [43] whereas  $\text{Cs}_2\text{CO}_3$  is reported to decompose in the temperature range of 823–873 K to  $\text{Cs}_2\text{O}$  [45]. Hence, although the alkali promoters may be below their melting points during the mixing of the components at elevated temperatures, the promoters are likely solubilized by the palmitic acid during synthesis of the promoted Cu–MgO catalysts, and this ensured that the promoters were well dispersed throughout the catalysts.

Fig. 3 shows the X-ray diffractograms of the MgO-based catalyst precursors, measured after calcination but prior to reduction. The data confirmed the presence of MgO (periclase, Fm3m(225)-cubic structure) and CuO (tenorite, C2/c(15) monoclinic structure) and the absence of  $\text{Cu}_2\text{O}$  in the precursor samples. In addition, no peaks associated with alkali metal oxides were observed, either because the alkali promoter was below the XRD detection limit (for the 0.5 wt% K and Cs samples) or they were present as amorphous, well dispersed alkali metal oxides (for the 4.4 wt% K and 13.5 wt% Cs samples). Using the data of Fig. 3, the MgO crystallite thickness ( $d_{\text{MgO}}^{\text{XRD}}$ ) and Cu crystallite thickness ( $d_{\text{Cu}}^{\text{XRD}}$ ) were estimated and the results are shown in Table 3. Both  $d_{\text{MgO}}^{\text{XRD}}$  and  $d_{\text{Cu}}^{\text{XRD}}$  increased in the same order that the  $S_{\text{BET}}$  of the MgO-based catalysts decreased, indicating that the loss in  $S_{\text{BET}}$  was also partly due to thermal sintering of the MgO and the Cu.

The unit cell size of the MgO ( $a_{\text{MgO}}$ ) was calculated from the XRD data for all of the MgO-based catalysts using the formula:  $a_{\text{MgO}} = 2d_{\text{MgO}}^{\text{XRD}}$  since MgO has a cubic crystal structure. As shown in Table 3, the same unit cell size was obtained for all of the catalysts, indicating that there was no solid solution present in the un-reduced Cu–MgO-based catalyst precursors. Hence it can be

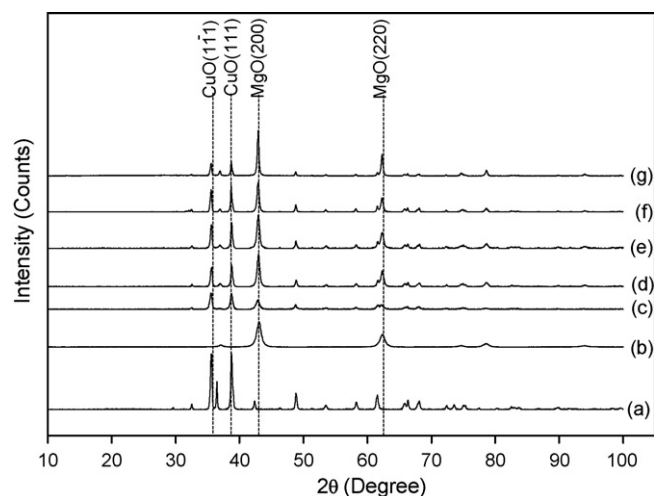


Fig. 3. X-ray diffractograms of un-reduced MgO-based catalysts: (a) CuO; (b) MgO; (c) Cu–MgO; (d) 0.5 wt% K–Cu–MgO; (e) 0.5 wt% Cs–Cu–MgO; (f) 4.4 wt% K–Cu–MgO; (g) 13.5 wt% Cs–Cu–MgO.

concluded that MgO and CuO crystallites were present as separate phases in the prepared catalysts.

The Cu dispersion of the Cu–MgO-based catalysts, reported in Table 3, show that for all of the catalysts the Cu dispersion was low (<2%). The Cu–MgO had the highest Cu dispersion among all of the prepared catalysts and addition of  $\text{K}_2\text{O}$  or  $\text{Cs}_2\text{O}$  decreased Cu dispersion. The Cu crystallite size ( $d_{\text{Cu}}^{\text{N}_2\text{O}}$ ) as inferred from the  $\text{N}_2\text{O}$  adsorption–decomposition analysis was significantly higher than that determined from the XRD analysis ( $d_{\text{Cu}}^{\text{XRD}}$ ), implying that most of the Cu crystallites (diameter < 30 nm), were occluded from the catalyst surface and not active to  $\text{N}_2\text{O}$  titration. The high Cu loading (>34.6 wt%) in the prepared Cu–MgO-based catalysts is the likely cause, resulting in significant agglomeration of CuO crystallites. Cu thermal sintering at the higher calcination temperatures used for the alkali-promoted Cu–MgO catalysts, compared to the unpromoted Cu–MgO catalyst, also contributed to the lower Cu dispersion of the alkali-promoted Cu–MgO compared to the unpromoted Cu–MgO.

The TPR profiles of the calcined catalyst precursors of the present study are reported in Fig. 4 and the reduction peak temperatures and calculated degrees of reduction are summarized in Table 4. For comparison, the TPR profiles of CuO and  $\text{Cu}_2\text{O}$  are also reported in Fig. 4 and Table 4. The CuO TPR profiles showed that bulk CuO had a reduction peak maximum at 516 K, in agreement with the literature [46]. The  $\text{Cu}_2\text{O}$  TPR profile showed a reduction peak maximum at 594 K. The degree of reduction for  $\text{Cu}_2\text{O}$  was 100% whereas the degree of reduction for CuO was 88%. The nominal particle size of all of the laboratory prepared catalysts as well as the bulk CuO of the present study was 267  $\mu\text{m}$ , whereas the  $\text{Cu}_2\text{O}$  particle size was 5  $\mu\text{m}$ . Hence it is likely that complete reduction of the CuO was hindered by  $\text{H}_2$  diffusion to the core of the larger, partially reduced Cu–CuO particle. Assuming CuO as the only reducible species present in the calcined catalyst precursors,

Table 3

Copper dispersion, crystallite size and MgO unit cell size of catalysts as determined by  $\text{N}_2\text{O}$  pulse titration and XRD.

Catalyst	Cu dispersion (%)	$S_{\text{Cu}}^{\text{N}_2\text{O}}$ ( $\text{m}^2 \text{g}^{-1}$ ) <sup>a</sup>	$d_{\text{Cu}}^{\text{N}_2\text{O}}$ (nm)	$d_{\text{Cu}}^{\text{XRD}}$ (nm)	$d_{\text{MgO}}^{\text{XRD}}$ (nm)	$a_{\text{MgO}}$ (nm)
MgO	–	–	–	–	13	0.42
Cu–MgO	1.54	2.64	65	15	17	0.42
0.5 wt% K–Cu–MgO	0.19	0.50	519	21	20	0.42
0.5 wt% Cs–Cu–MgO	0.28	0.58	362	24	20	0.42
4.4 wt% K–Cu–MgO	0.24	0.60	420	26	24	0.42
13.5 wt% Cs–Cu–MgO	0.52	0.76	194	27	32	0.42

<sup>a</sup> Copper metal surface area was calculated assuming  $1.46 \times 10^{19}$  copper atoms per  $\text{m}^2$ .

**Table 4**  
Temperature-programmed reduction results for Cu–MgO-based catalysts.

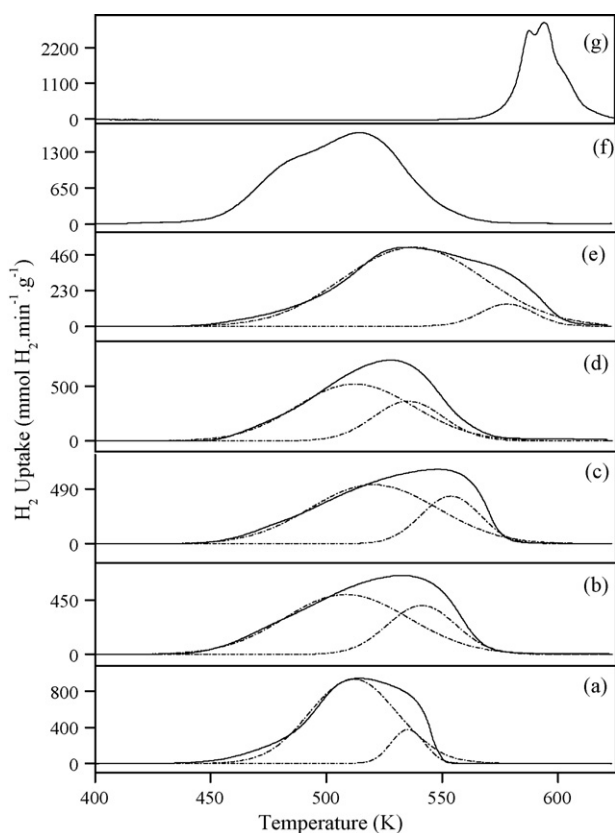
Sample	Hydrogen consumption (mmol g <sup>-1</sup> catalyst)	Distribution of different copper oxide species <sup>a</sup> (%)		Degree of reduction (%)	Reduction peak temperature (K)	
		1	2		T <sub>1</sub>	T <sub>2</sub>
Cu <sub>2</sub> O	6.84	100	–	100	594	–
CuO	11.06	100	–	88	516	–
Cu–MgO	5.08	87	13	88	512	535
0.5 wt% K–Cu–MgO	4.77	69	31	83	506	539
0.5 wt% Cs–Cu–MgO	4.89	73	27	85	518	552
4.4 wt% K–Cu–MgO	4.56	71	29	83	512	535
13.5 wt% Cs–Cu–MgO	4.20	90	10	84	538	578

<sup>a</sup> Copper oxide species corresponded to CuO in all cases except for Cu<sub>2</sub>O catalyst.

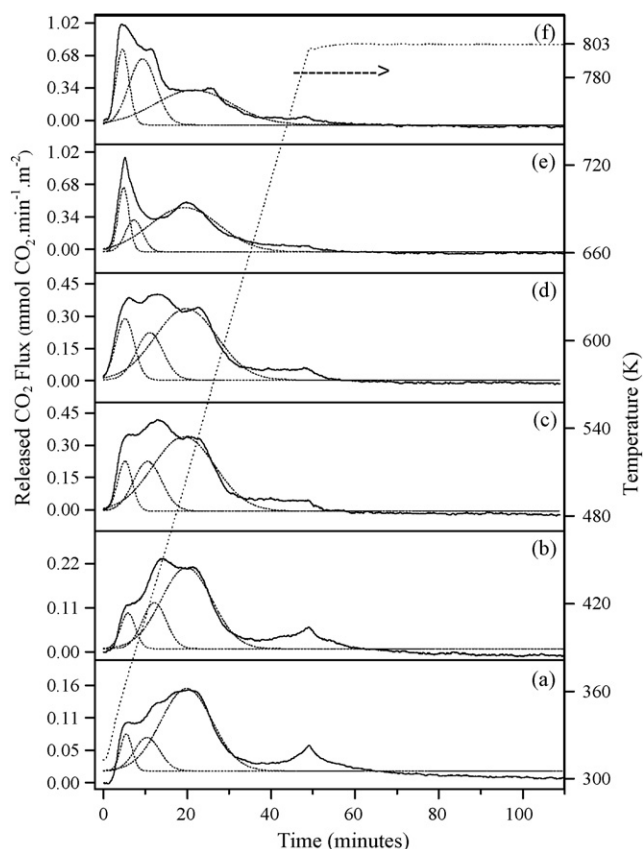
the TPR results of the Cu–MgO-based catalysts revealed that, in all cases, the degree of reduction was more than 80%. However, due to an interaction between the alkali metal oxide, the MgO and the CuO, 100% reduction of the CuO was not achieved and two different reduction temperatures were observed. The TPR profiles were therefore de-convoluted (Fig. 4) to quantify each of the CuO species. Except for the 13.5 wt% Cs–Cu–MgO, the first reduction peak occurred in the range of 506–518 K and the second reduction peak occurred in the range of 535–552 K. The first reduction peak was attributed to bulk CuO reduction and the second was assigned to CuO species that interacted with MgO and/or the alkali promoters and were consequently, more difficult to reduce. The weak CuO interaction with bulk MgO and its inhibiting effect on Cu reduction has been reported previously [46–48]. Addition of the alkali promoters to Cu–MgO led to more CuO species that were more difficult to reduce, indicative of the K<sub>2</sub>O and Cs<sub>2</sub>O interaction with the CuO. The phenomenon of alkali metal oxide interaction

with CuO and its inhibiting effect on CuO reduction, has also been noted in previous studies [49] and is apparent for all the alkali-promoted Cu–MgO catalysts reported in Table 4. The TPR profile of the 0.5 wt% K–Cu–MgO showed reduction peaks at 506 K and 539 K with a significant increase in the CuO species reduced at high temperature compared to the case of Cu–MgO. The TPR profile of the 0.5 wt% Cs–Cu–MgO showed reduction peaks at 518 K and 552 K and although these temperatures were slightly higher than for the 0.5 wt% K–Cu–MgO, the relative amounts of the two types of CuO species were very similar. Comparison of the TPR profile for 0.5 wt% K–Cu–MgO and 4.4 wt% K–Cu–MgO showed almost identical results, suggesting that increased K loading did not influence the interaction of K<sub>2</sub>O with the CuO. However, the TPR profile of the 13.5 wt% Cs–Cu–MgO showed reduction peaks at 538 K and 578 K, significantly higher than for the other catalysts of Table 4. The first reduction peak was most likely due to the Cs<sub>2</sub>O interaction with CuO described earlier. It is noticeable that except for the case of 13.5 wt% Cs–Cu–MgO, all of the Cu–MgO-based catalysts showed reduction peaks below the Cu<sub>2</sub>O reduction peak temperature. This suggests that the high loading of Cs (13.5 wt%) led to the formation of a small amount of Cu<sub>2</sub>O (<10 wt%) in the Cs–Cu–MgO catalyst that was not detectable by XRD, but that led to the second reduction peak in the TPR profile that corresponded to the reduction peak for bulk Cu<sub>2</sub>O. The non-Gaussian TPR profile of the Cu–MgO-based catalysts (Fig. 4) has been attributed to different copper oxide species present in the catalyst that reduce at different temperatures (Table 4). However, the presence of a heterogeneous size distribution of copper particles in the Cu–MgO catalyst may also contribute to the shape of the TPR curves, although in this case, higher N<sub>2</sub>O uptakes from the smallest reduced Cu species would be expected to yield much higher overall N<sub>2</sub>O uptakes than that reported in Table 3.

The CO<sub>2</sub> TPD profiles for all of the catalysts, shown in Fig. 5, were used to determine the catalyst intrinsic basicity and distribution of basic sites, as summarized in Table 5. The intrinsic basicity increased in the order: MgO < Cu–MgO < 0.5 wt% K–Cu–MgO < 0.5 wt% Cs–Cu–MgO < 4.4 wt% K–Cu–MgO < 13.5 wt% Cs–Cu–MgO and follows the expected trend, based on the known basicities of K, Cs and MgO. MgO had an intrinsic basicity of 2.7 μmol CO<sub>2</sub> m<sup>-2</sup> in agreement with the MgO basicity reported in the literature [32–35]. Addition of Cu to the MgO increased the intrinsic basicity but the distribution of basic sites was almost unchanged. Addition of alkali metal (0.5 wt% Cs or K) to the Cu–MgO catalyst more than doubled the intrinsic basicity but the distribution of basic sites remained almost unchanged. The 4.39 wt% K–Cu–MgO catalyst had higher intrinsic basicity compared to the 0.50 wt% K–Cu–MgO catalyst, as well as a slightly higher percentage of weak basic sites, and similar trends were observed for the Cs–Cu–MgO catalyst. Therefore it can be concluded that in all cases, addition of alkali promoter to the Cu–MgO catalyst increased the intrinsic basicity but the effect on the distribution of basic sites was much less significant.



**Fig. 4.** Temperature program reduction profile for: (a) 40.1Cu–MgO; (b) 0.5 wt% K–Cu–MgO; (c) 0.5 wt% Cs–Cu–MgO; (d) 4.4 wt% K–Cu–MgO; (e) 13.5 wt% Cs–Cu–MgO; (f) CuO; (g) Cu<sub>2</sub>O.



**Fig. 5.** CO<sub>2</sub> temperature program desorption of (a) MgO; (b) Cu–MgO; (c) 0.5 wt% K–Cu–MgO; (d) 0.5 wt% Cs–40.1 Cu–MgO; (e) 4.4 wt% K–Cu–MgO; (f) 13.5 wt% Cs–Cu–MgO.

The basicity of an oxide surface is generally related to the electron donating properties of the combined oxygen anions, so that the higher the partial negative charge on the combined oxygen anions, the more basic the oxide. Therefore, the oxygen partial negative charge reflects the electron donor properties of the oxygen in a single component oxide. Lopez et al. [50] suggested that Cu bonds ionically to MgO and forms a stable Cu–O–Mg species. These authors claimed that Cu gains a large net positive charge while the Cu electron is transferred to MgO. This more likely leads to an increase in the oxygen partial negative charge in MgO and could explain the increase in the catalyst basic site density after Cu addition to MgO. The oxygen partial negative charge increased in the order Cs<sub>2</sub>O > K<sub>2</sub>O > MgO according to calculations made by Diez et al. [40,42]. The basicity trend of the present study is in good agreement with these calculations.

Since the catalyst basicity is expected to play an important role in the formation of the first C–C bond in ethanol synthesis from syngas and methanol [14,24–28] a comparison of the basicity of the present catalysts to conventional Cu–ZnO-based catalysts is

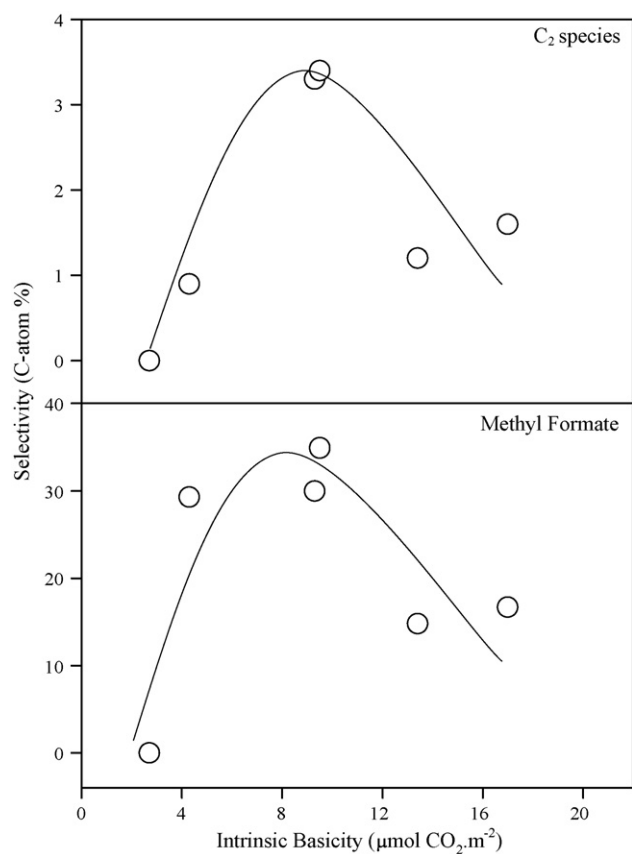
important. Cu–ZnO–Zr<sub>2</sub>O (Cu wt% = 41.20) has a reported intrinsic basicity of 0.4 μmol CO<sub>2</sub> m<sup>-2</sup> [36], whereas in the present study the Cu–MgO intrinsic basicity was 4.3 μmol CO<sub>2</sub> m<sup>-2</sup>. The intrinsic basicity of the Cu–MgO catalyst of the present study is approximately 11 times higher than that of Cu–ZnO–Zr<sub>2</sub>O [36]. Addition of K or Cs to the Cu–MgO increased the intrinsic basicity further, with a value of 9.3 μmol CO<sub>2</sub> m<sup>-2</sup> obtained for the 0.5 wt% K–Cu–MgO catalyst. The corresponding value for a 0.5 wt% K promoted Cu–ZnO–Al<sub>2</sub>O<sub>3</sub> catalyst, measured at 196 K, was reported as 2.7 μmol CO<sub>2</sub> m<sup>-2</sup> [12].

### 3.2. Product distribution over MgO-based catalyst

Previous work suggested that the formation of higher alcohols over Cu–ZnO-based catalysts is favoured at low H<sub>2</sub>/CO ratios (<1) [12,23,51,52]. Furthermore, isotopic tracer studies and NMR studies of ethanol synthesis from syngas and methanol over Cu–ZnO-based catalysts, suggested that CO is the main source of carbon in ethanol formation [27], whereas others have suggested that methanol is the main source of carbon in ethanol formation [14]. Hence, in the present work, initial catalyst testing was done in a CH<sub>3</sub>OH/CO feed in the absence of H<sub>2</sub>. The catalysts were tested at 101 kPa, 498 K, with a feed composition of He/CO/CH<sub>3</sub>OH = 0.20/0.66/0.14 (molar) and contact time (*W/F*) of 12.3 × 10<sup>-3</sup> g min (cm<sup>3</sup>(STP))<sup>-1</sup>. A summary of the product distribution and net conversion of reactants is given in Table 6. As expected, the total conversion of reactants over MgO was very low, whereas addition of Cu and alkali oxide to MgO increased the total conversion significantly. Note that in most cases the net CO consumption was negative, implying that the amount of CO incorporated into the formation of different carbonaceous products was less than the amount of CO generated by CH<sub>3</sub>OH decomposition. In these cases, CO was treated as a product and its selectivity was included in the product selectivity calculations. The data of Table 6 show that the CO selectivity (*S*<sub>CO</sub>) at 498 K decreased in the order: Cu–MgO > 0.5 wt% K–Cu–MgO > 0.5 wt% Cs–Cu–MgO, whereas the reverse order was observed for methyl formate (*S*<sub>MF</sub>), CO<sub>2</sub> (*S*<sub>CO<sub>2</sub></sub>) and C<sub>2</sub> (*S*<sub>C<sub>2</sub></sub>) selectivities. The catalyst intrinsic basicity (Table 5) increased in the order Cu–MgO < 0.5 wt% K–Cu–MgO < 0.5 wt% Cs–Cu–MgO. Thus it can be concluded that an increase in the density of basic sites increased *S*<sub>MF</sub> and *S*<sub>C<sub>2</sub></sub>. However, comparing the 0.5 wt% K–Cu–MgO and the 4.4 wt% K–Cu–MgO as well as the 0.5 wt% Cs–Cu–MgO and the 13.5 wt% Cs–Cu–MgO catalysts, shows that increased K or Cs loading increased the *S*<sub>CO</sub> and decreased in *S*<sub>MF</sub> and *S*<sub>C<sub>2</sub></sub>. Intrinsic basicity, however, increased with increased alkali metal loading (Table 5). Hence, among these catalysts, increased basic site density decreased *S*<sub>MF</sub> and *S*<sub>C<sub>2</sub></sub> and increased *S*<sub>CO</sub>. Together, these data suggest that an optimum intrinsic basicity exists that maximizes selectivity to methyl formate and C<sub>2</sub> product species, as shown in Fig. 6. Note that changes in the catalyst intrinsic basicity were unavoidably accompanied by changes in Cu dispersion, *S*<sub>BET</sub>, *V*<sub>p</sub> and their impact on *S*<sub>MF</sub>, *S*<sub>C<sub>2</sub></sub> and *S*<sub>CO</sub> is reflected in the scatter of the data of Fig. 6.

**Table 5**  
Basic properties of MgO-based catalyst measured by means of CO<sub>2</sub> TPD.

Catalyst	Specific basicity (μmol CO <sub>2</sub> g <sup>-1</sup> )	Intrinsic basicity (μmol CO <sub>2</sub> m <sup>-2</sup> )	Distribution of different basic sites on the catalyst (%)		
			Weak	Medium	Strong
MgO	432.0	2.7	8	15	77
Cu–MgO	315.5	4.3	9	19	72
0.5 wt% K–Cu–MgO	392.4	9.3	11	21	69
0.5 wt% Cs–Cu–MgO	415.9	9.5	16	19	65
4.4 wt% K–Cu–MgO	403.0	13.4	16	13	71
13.5 wt% Cs–Cu–MgO	305.7	17.0	18	33	49



**Fig. 6.** Selectivity from reaction of CH<sub>3</sub>OH/CO over alkali-promoted Cu–MgO catalysts as a function of their intrinsic basicity. Reaction conditions: 101 kPa, 498 K, feed composition He/CO/CH<sub>3</sub>OH = 0.20/0.66/0.14 (molar) W/F = 12.3 × 10<sup>-3</sup> min g (cm<sup>3</sup>(STP))<sup>-1</sup>, catalyst weight = 0.98 g.

The product distribution over the 0.5 wt% K–Cu–MgO and the 0.5 wt% Cs–Cu–MgO catalysts at 498 K and 523 K (Table 6), show that increased temperature increased  $S_{\text{CO}}$  whereas  $S_{\text{MF}}$  and  $S_{\text{C}_2}$  decreased, implying that lower operating temperature favoured C<sub>2</sub> species formation.

Since the 0.5 wt% Cs–Cu–MgO catalyst showed the highest selectivity towards C<sub>2</sub> species among all the tested catalysts, further experiments were conducted as a function of contact time (W/F) using this catalyst and the results are presented in Fig. 7. Also, to study the effect of Cs loading on the performance of the Cs promoted Cu–MgO catalyst, the same series of contact time experiments was performed on the 13.5 wt% Cs–Cu–MgO, and the results are

shown in Fig. 8. For both the 0.5 wt% Cs–Cu–MgO and the 13.5 wt% Cs–Cu–MgO catalysts, it was observed that decreased contact time led to increased  $S_{\text{MF}}$  and decreased  $S_{\text{CO}}$ , whereas the  $S_{\text{C}_2}$  and  $S_{\text{CO}_2}$  remained almost unchanged. These observations imply that methyl formate was a primary product over both catalysts whereas CO was a secondary product, in agreement with previous studies [53,54].

The effect of different feed mixtures on the product distribution over the 13.5 wt% Cs–Cu–MgO catalyst was also examined using a feed of Ar/He/CH<sub>3</sub>OH, CO/He/CH<sub>3</sub>OH and H<sub>2</sub>/He/CH<sub>3</sub>OH and the results are shown in Table 7. The presence of either H<sub>2</sub> or CO in the feed stream compared to Ar, decreased the total conversion and the decrease in total conversion was more significant in the presence of H<sub>2</sub> than CO. Furthermore, the presence of H<sub>2</sub> in the feed decreased  $S_{\text{MF}}$  marginally, whereas the presence of CO in the feed, increased the  $S_{\text{MF}}$  compared to the presence of Ar in the feed.  $S_{\text{C}_2}$  decreased in the following order: H<sub>2</sub>/He/CH<sub>3</sub>OH > CO/He/CH<sub>3</sub>OH > Ar/He/CH<sub>3</sub>OH revealing that the presence of H<sub>2</sub>, as opposed to CO and Ar in the feed, improved  $S_{\text{C}_2}$ , but note that the CH<sub>3</sub>OH conversion decreased significantly in the H<sub>2</sub> rich atmosphere.

#### 4. Discussion

The present study has demonstrated the preparation of high surface area MgO by thermal decomposition of Mg(NO<sub>3</sub>)<sub>2</sub> in the presence of palmitic acid, and this method has been extended to alkali-promoted Cu–MgO catalysts. Using CO<sub>2</sub> TPD to quantify basicity, the alkali-promoted Cu–MgO was shown to have a higher intrinsic basicity than conventional Cu–ZnO catalysts and alkali-promoted Cu–ZnO catalysts. The surface area of the MgO (160 m<sup>2</sup> g<sup>-1</sup>) was significantly higher than the Cu–MgO (74 m<sup>2</sup> g<sup>-1</sup>), due mostly to pore blocking by the Cu. Further losses in surface area upon alkali promotion were shown to be due to both pore blocking and sintering effects. The latter was due to the higher calcination temperatures of the alkali promoted catalysts compared to the Cu–MgO.

Several reaction mechanisms have been proposed for the conversion of syngas to CH<sub>3</sub>OH and other oxygenated products as well as for the conversion of CH<sub>3</sub>OH to methyl formate, C<sub>2</sub> species (mainly ethanol), CO and CO<sub>2</sub>. A summary of the most consistent mechanisms proposed in the literature regarding the formation of these products over Cu/metal oxide catalysts is shown in Figs. 9–11. In order to simplify these figures, the reaction pathways and intermediates containing carbon atoms are shown, whereas H, OH, H<sub>2</sub>O and H<sub>2</sub> species are omitted. Results from the present study are conveniently discussed in view of some of these mechanistic proposals.

The present work showed that at 498 K on the high surface area MgO (Table 6) only, a small amount of the feed CH<sub>3</sub>OH was con-

**Table 6**  
Product distribution and catalyst activity over MgO-based catalysts using CO/He/CH<sub>3</sub>OH feed.

Catalyst	Reaction temperature (K)	Net CO consumption (C-atom %)	Net CH <sub>3</sub> OH conversion (C-atom %)	Total net conversion <sup>a</sup> (C-atom %)	Product selectivity (C-atom %)			
					CO	MF <sup>b</sup>	CO <sub>2</sub>	C <sub>2</sub> <sup>c</sup>
MgO	498	-1.2	6.4	5.3	100.0	0.0	0.0	0.0
Cu–MgO	498	-9.7	84.7	75.0	68.4	29.3	1.5	0.9
0.5 wt% K–Cu–MgO	498	-7.9	70.0	62.0	63.9	30.0	2.7	3.3
	523	-10.8	81.8	71.0	78.2	16.9	2.9	2.1
0.5 wt% Cs–Cu–MgO	498	-6.1	66.7	60.6	53.4	34.9	8.4	3.4
	523	-12.5	87.0	74.5	84.3	10.3	2.9	2.5
4.4 wt% K–Cu–MgO	498	-10.0	70.1	60.2	82.9	14.8	1.1	1.2
13.5 wt% Cs–Cu–MgO	498	-6.3	47.2	40.8	79.8	16.7	1.9	1.6

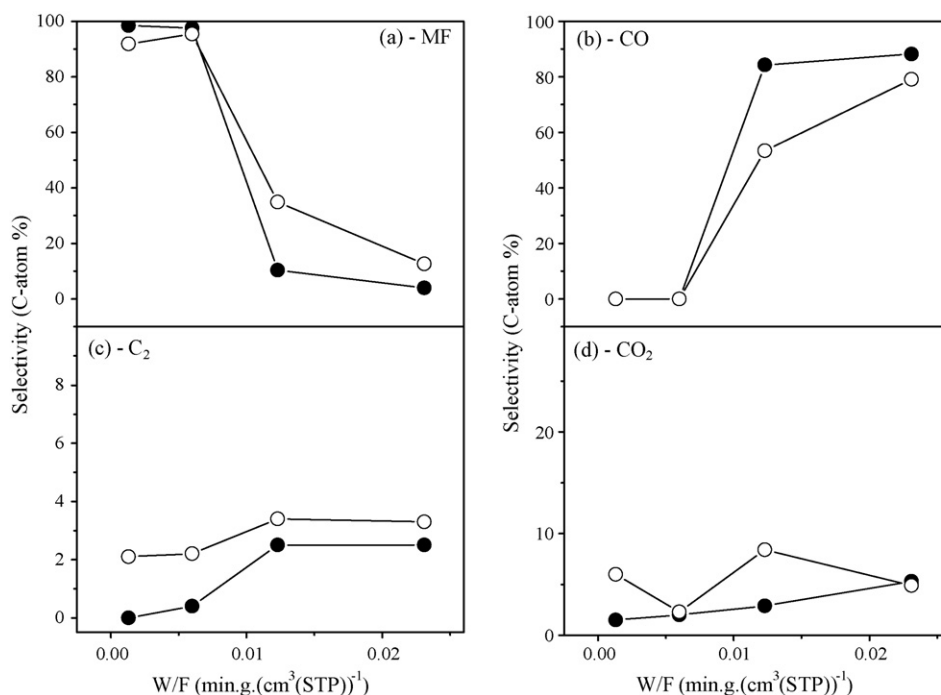
Reaction condition: 101 kPa, feed He/CO/CH<sub>3</sub>OH = 0.20/0.66/0.14 molar, contact time (W/F) = 12.3 × 10<sup>-3</sup> min g (cm<sup>3</sup>(STP))<sup>-1</sup>, catalyst weight = 0.98 g, v<sub>0</sub> = 84.4 cm<sup>3</sup>(STP) min<sup>-1</sup>.

<sup>a</sup> Total conversion = Net CO consumption + Net CH<sub>3</sub>OH conversion.

<sup>b</sup> MF stands for methyl formate.

<sup>c</sup> C<sub>2</sub> stands for ethanol and acetic acid.

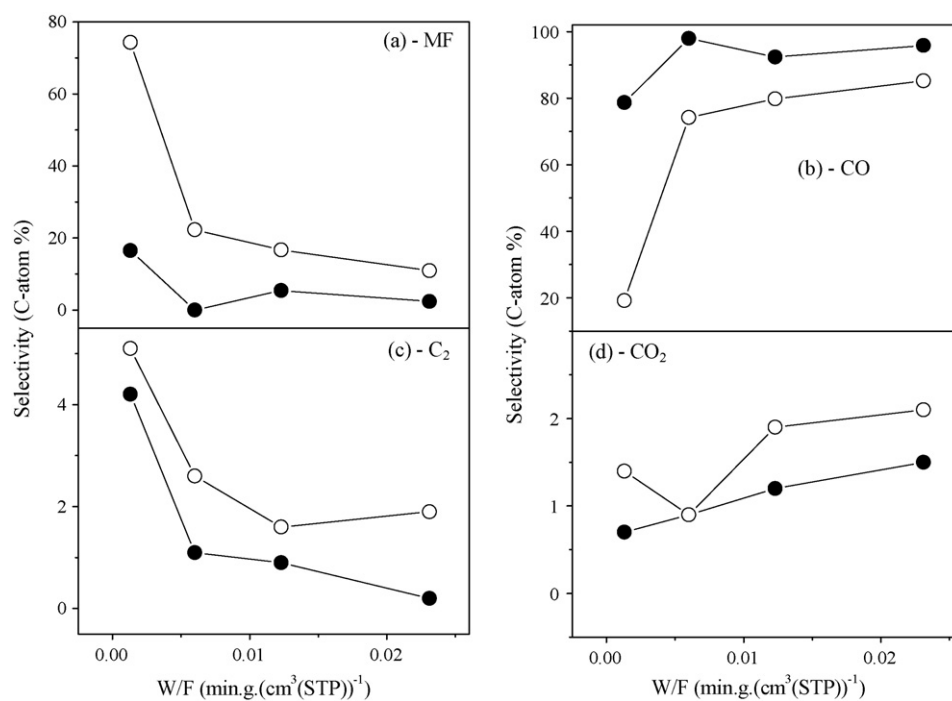




**Fig. 7.** Selectivity from reaction of  $\text{CH}_3\text{OH}/\text{CO}$  over 0.5 wt% Cs-Cu-MgO at (○) 498 K and (●) 523 K as a function of contact time ( $W/F$ ) for: (a) methyl formate, (b) CO, (c) acetic acid and ethanol, (d)  $\text{CO}_2$ . Reaction conditions: 101 kPa, feed composition  $\text{He}/\text{CO}/\text{CH}_3\text{OH} = 0.20/0.66/0.14$  (molar),  $v_0 = 84.4 \text{ cm}^3(\text{STP}) \text{ min}^{-1}$ .

verted to CO but no methyl formate, dimethyl ether (DME), other  $\text{C}_2$  oxygenates or  $\text{CO}_2$  was produced. Addition of Cu to the MgO resulted in a significant increase in conversion (from 5.3 to 75.0%, Table 6), with a high selectivity to methyl formate (29.3%) and CO (68.4%), and a low  $\text{CO}_2$  (1.5%) and  $\text{C}_2$  (0.9%) selectivity. Addition of the alkali promoters resulted in changes in the product selectivity, but in all cases, CO and methyl formate remained the major products. Clearly, although the basic MgO is able to convert  $\text{CH}_3\text{OH}$  to

CO, most likely through the methoxy species shown in Path A-1 of Fig. 9, Cu is needed to obtain products other than CO. However, there is a well established synergy between the Cu and the metal oxide present in the catalyst [37] that influences product selectivity. In the present work, the basic MgO and alkali promoters ensure that no dimethyl ether is formed [30,37], and the selectivities to methyl formate,  $\text{CO}_2$  and  $\text{C}_2$  oxygenates were all dependent on the catalyst formulation (Table 6). Furthermore, both the reaction temperature



**Fig. 8.** Selectivity from reaction of  $\text{CH}_3\text{OH}/\text{CO}$  over 13.5 wt% Cs-Cu-MgO at (○) 498 K and (●) 523 K as a function of contact time ( $W/F$ ) for: (a) methyl formate, (b) CO, (c) acetic acid and ethanol, (d)  $\text{CO}_2$ . Reaction conditions: 101 kPa, feed composition  $\text{He}/\text{CO}/\text{CH}_3\text{OH} = 0.20/0.66/0.14$  (molar),  $v_0 = 84.4 \text{ cm}^3(\text{STP}) \text{ min}^{-1}$ .

**Table 7**  
Product distribution and catalyst activity over 13.5 wt% Cs–Cu–MgO in different feed compositions.

Reaction temperature (K)	Feed mixture	Net CO consumption (C-atom %)	Net CH <sub>3</sub> OH conversion (C-atom %)	Total conversion <sup>a</sup> (C-atom %)	Product selectivity (C-atom %)			
					CO	MF <sup>b</sup>	CO <sub>2</sub>	C <sub>2</sub> <sup>c</sup>
498	Ar/He/CH <sub>3</sub> OH	0.0	48.2	48.2	81.7	15.2	2.9	0.2
	CO/He/CH <sub>3</sub> OH	-6.3	47.2	40.8	79.8	16.7	1.9	1.6
	H <sub>2</sub> /He/CH <sub>3</sub> OH	0.0	6.6	6.6	79.5	13.6	3.3	3.6
523	Ar/He/CH <sub>3</sub> OH	0.0	62.1	62.1	97.6	1.6	0.8	0.0
	CO/He/CH <sub>3</sub> OH	-7.3	47.0	39.7	92.4	5.4	1.2	0.9
	H <sub>2</sub> /He/CH <sub>3</sub> OH	0.0	22.8	22.8	96.1	1.6	1.1	1.2

Reaction condition: 101 kPa, feed X/He/CH<sub>3</sub>OH = 0.20/0.66/0.14 molar, where X is Ar or CO or H<sub>2</sub>, contact time (W/F) = 12.3 × 10<sup>-3</sup> min g (cm<sup>3</sup>(STP))<sup>-1</sup>, catalyst weight = 0.98 g, v<sub>0</sub> = 84.4 cm<sup>3</sup>(STP) min<sup>-1</sup>.

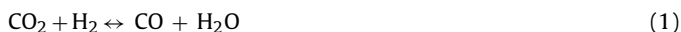
<sup>a</sup> Total conversion = Net CO consumption + Net CH<sub>3</sub>OH conversion.

<sup>b</sup> MF stands for methyl formate.

<sup>c</sup> C<sub>2</sub> stands for ethanol and acetic acid.

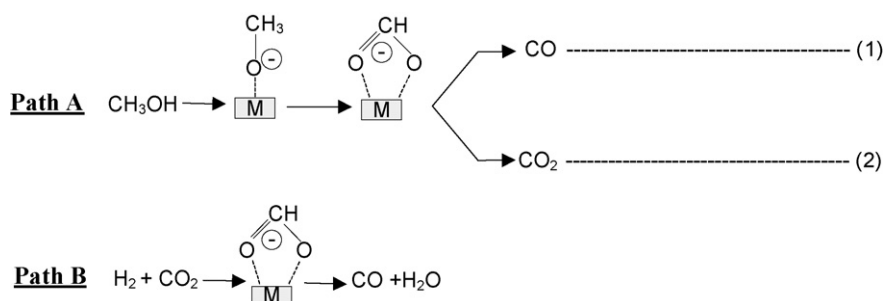
and space velocity had a significant effect on the product selectivity. The data of Table 6 show that increased temperature resulted in higher methanol conversion and CO selectivity, with reduced selectivity to methyl formate and other C<sub>2</sub> oxygenates. Figs. 7 and 8 suggest that the initial product of reaction over the Cs–Cu–MgO catalyst was methyl formate, while CO was a secondary product. The selectivity to CO<sub>2</sub> was not a strong function of operating conditions.

Studies using <sup>13</sup>CO and <sup>13</sup>CO<sub>2</sub> and H<sub>2</sub> as reactant have shown that CH<sub>3</sub>OH is produced mainly from CO<sub>2</sub> and H<sub>2</sub> rather than CO and H<sub>2</sub> on Cu catalysts [10]. Hence, the methanol synthesis on Cu-based catalysts can be described by the following two parallel reactions [26,29]:

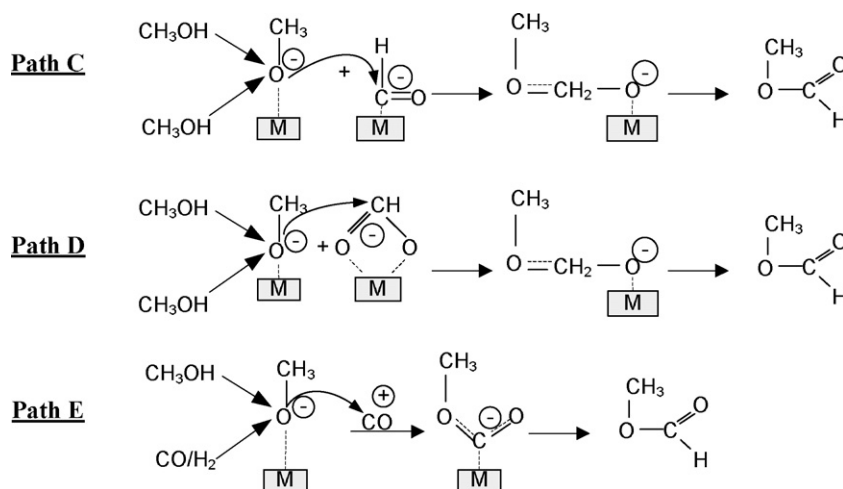


Most of the mechanistic studies on Cu catalysts agree that a formate species is formed from H<sub>2</sub> and CO<sub>2</sub> and further surface reaction leads to products CH<sub>3</sub>OH and H<sub>2</sub>O (the reverse of Path A-2 of Fig. 9) or CO and H<sub>2</sub>O (Path B of Fig. 9) [24,26,29]. Carbon isotopic tracer studies have shown that the rate of the reverse water gas shift (Reaction (1)) is higher than the rate of CH<sub>3</sub>OH synthesis from CO<sub>2</sub>/H<sub>2</sub> (Reaction (2)) [29]. In the present work, no H<sub>2</sub>O was added in the feed and consequently the reverse of Reaction (2) could not occur to any great extent. However, the data of Figs. 7 and 8 show that even at high space velocities some C<sub>2</sub> oxygenates were produced, and water is a co-product of these reactions. Consequently, the reverse of both Reactions (1) and (2) occur but to a limited extent because of the low levels of water generated as a consequence of C<sub>2</sub> formation. In the presence of water it is likely that a portion of the CH<sub>3</sub>OH present in the feed decomposed to CO<sub>2</sub> via Path A-2 of Fig. 9. Alternatively, the forward or reverse reaction shown as Path B of Fig. 9 could occur, although this seems less likely in the present work given that the amount of CO<sub>2</sub> was not strongly dependent on the CO present in the feed (Table 7), nor on the C<sub>2</sub> selectivity (Figs. 7 and 8).

CH<sub>3</sub>OH conversion to methyl formate over Cu-based catalysts has been well studied and it is known that Cu plays a significant role as active catalyst for methyl formate formation [29,30,54]. Fig. 10 shows potential routes to methyl formate, but the mechanisms that have received the most acceptance are the CH<sub>3</sub>OH dimerization paths shown as Path C and D. Recent evidence based on H/D exchange experiments [55] and experiments using <sup>13</sup>C labelled methanol [56] suggested that methyl formate is generated via the nucleophilic attack of a surface methoxy species on a surface formyl species (Path C of Fig. 10) or a formate species (Path D of Fig. 10) [30,53–56]. Nunan et al. [14] provided thermodynamic and other arguments to suggest that methyl formate was generated by methanol carbonylation over their Cs–Cu–ZnO catalyst operated at high pressure (7.6 MPa). At the low pressure conditions of the present study, however, the methyl formate generated was about three orders of magnitude greater than the equilibrium yield from methanol carbonylation (CH<sub>3</sub>OH + CO → HCOOCH<sub>3</sub>,  $K_{\text{Eq}}^{598\text{K}} = 2.11 \times 10^{-4}$  versus  $K_{\text{Calc}}^{598\text{K}} = 3.45 \times 10^{-1}$ ), whereas it was less than the methanol dimerization equilibrium yield (2CH<sub>3</sub>OH → HCOOCH<sub>3</sub> + 2H<sub>2</sub>,  $K_{\text{Eq}}^{598\text{K}} = 3.14 \times 10^{-2}$  versus  $K_{\text{Calc}}^{598\text{K}} = 2.22 \times 10^{-2}$ ). The methanol dimerization reaction to methyl formate and hydrogen could occur directly from methoxy and formyl species derived from CH<sub>3</sub>OH interacting with Cu as well as the basic sites of the present catalysts. Other studies on the effect of the state of Cu on methyl formate formation have suggested that CH<sub>3</sub>OH decomposes to CO via a methyl formate intermediate over Cu<sup>0</sup>, but no clear mechanism was proposed for this step [53,54]. In the present work it is likely that surface formyl, methoxy and formate all exist on the catalyst surface. Path C and Path D of Fig. 10 yield methyl formate as a primary product. Subsequent decomposition of methyl formate to CH<sub>3</sub>OH and CO, or to CO and H<sub>2</sub>, would yield CO as a secondary product, in agreement with the experimental observations of Figs. 7 and 8. Hence it is likely that in the present study, part of the CH<sub>3</sub>OH present in the feed stream was decomposed to CO via methyl formate over Cu<sup>0</sup>.



**Fig. 9.** Pathway for: (A-1) CH<sub>3</sub>OH decomposition to CO, (A-2) CH<sub>3</sub>OH decomposition to CO<sub>2</sub> [24,26,29], (B) reverse water gas shift [29]. M stands for Cu<sup>0</sup> or metal cation.

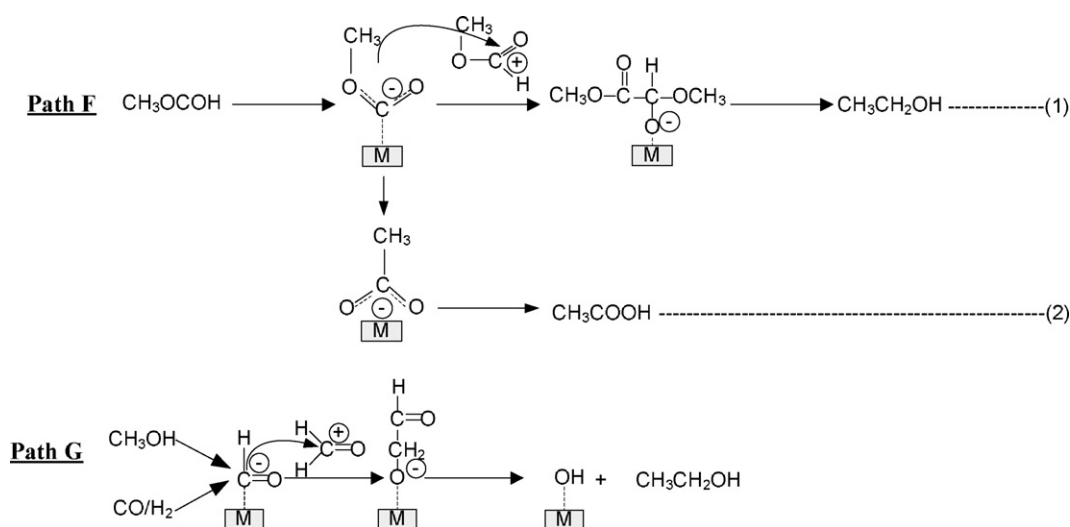


**Fig. 10.** Pathway for: (C)  $\text{CH}_3\text{OH}$  dimerization to methyl formate via methoxy and formyl intermediates [55,56], (D)  $\text{CH}_3\text{OH}$  dimerization to methyl formate via methoxy and formate intermediates [55,56], (E)  $\text{CH}_3\text{OH}$  carbonylation to methyl formate [14]. M stands for  $\text{Cu}^0$  or metal cation.

Results of the present work showed that an increase in catalyst intrinsic basicity up to  $9.5 \mu\text{mol CO}_2 \text{ m}^{-2}$  at low Cu dispersion ( $<1.54\%$ ), led to an increase in  $S_{\text{MF}}$  (Fig. 6). The methyl formate selectivity decreased in the order:  $0.5 \text{ wt}\% \text{ Cs-Cu-MgO} > 0.5 \text{ wt}\% \text{ K-Cu-MgO} \approx \text{Cu-MgO}$ . Also, addition of CO to  $\text{CH}_3\text{OH}$  in the feed led to a small increase in  $S_{\text{MF}}$ . The formation of methyl formate via nucleophilic attack by methoxide species on formyl species would be enhanced by increased basicity of the catalyst, as has been observed. An increase in catalyst intrinsic basicity also led to a small increase in  $S_{\text{C}_2}$ . Xu and Iglesias [27] have suggested that nucleophilic attack of the methyl formate by surface  $\text{CH}_3\text{OCO}^-$  species on a basic catalyst (metal cation) leads to the formation of an initial C–C bond that yields ethanol following several hydrogenation steps that are not shown in Path F-1 of Fig. 11. Other mechanistic studies suggest that the nucleophilic attack of an adsorbed formyl species with formaldehyde on a basic site leads to the formation of the initial C–C bond which subsequently yields ethanol (Path G of Fig. 11) [14]. Noting that formaldehyde was absent in both the feed and product streams of the present study, it is likely an increase in the catalyst intrinsic basicity led to a nucleophilic

attack of the methyl formate by surface  $\text{CH}_3\text{OCO}^-$  species on a basic site, leading to ethanol formation and a small increase in  $\text{C}_2$  formation ( $S_{\text{C}_2} < 5 \text{ C-atom}\%$ ). Results of the present work showed that  $S_{\text{C}_2}$  decreased in the order:  $0.5 \text{ wt}\% \text{ Cs-Cu-MgO} \approx 0.5 \text{ wt}\% \text{ K-Cu-MgO} > \text{Cu-MgO}$  suggesting that Path F-1 of Fig. 11 took place over  $\text{Cu/Mg}^{2+}$  and addition of  $\text{Cs}_2\text{O}$  and  $\text{K}_2\text{O}$  to  $\text{Cu-MgO}$  provided stronger basic sites ( $\text{Cs}^+$  and  $\text{K}^+$ ) for this reaction pathway.

To the authors knowledge, only one previous study has reported the formation of acetic acid from  $\text{CH}_3\text{OH}/\text{CO}$  over Cu-based catalysts [14]. The only mechanistic studies available for acetic acid synthesis suggest that nucleophilic attack of CO on methoxide over a basic site leads to  $\text{CH}_3\text{OCO}^-$  species. The rearrangement of  $\text{CH}_3\text{OCO}^-$  species to acetate species ( $\text{CH}_3\text{COO}^-$ ) leads to C–C bond formation, and a final hydrogenation step yields acetic acid (Path F-2 of Fig. 11) [14]. However, Nunan et al. [14] noted that the rearrangement step ( $\text{CH}_3\text{OCO}^- \rightarrow \text{CH}_3\text{COO}^-$ ) had high activation energy (based on an analysis of gas phase reactions) and was not very likely to occur. In the present study, the increase in the catalyst intrinsic basicity up to  $7.5 \mu\text{mol CO}_2 \text{ m}^{-2}$  led to a small



**Fig. 11.** Pathway for: (F-1) ethanol formation from methyl formate [27], (F-2) acetic acid formation from methyl formate [14], (G) ethanol formation from  $\text{CH}_3\text{OH}$  and CO [14]. M stands for  $\text{Cu}^0$  or metal cation.

increase in the  $S_{C_2}$  and it is likely that the high intrinsic basicity of the alkali-promoted Cu–MgO catalysts facilitated the formation of small amounts of acetic acid (acetic acid selectivity < 3 C-atom %) on the catalyst surface as shown by Path F-2 of Fig. 11.

The correlation between intrinsic basicity and  $S_{MF}$ ,  $S_{C_2}$  and  $S_{CO}$  identified in the present study (Fig. 6), suggests that at low Cu dispersion (<1.54%), an increase in the intrinsic basicity up to  $9.5 \mu\text{mol CO}_2 \text{ m}^{-2}$ , leads to an increase in  $S_{MF}$  and  $S_{C_2}$ , while a further increase in the intrinsic basicity leads to a decrease in  $S_{MF}$  and  $S_{C_2}$ . (In both cases the opposite trend was observed for  $S_{CO}$  compared to  $S_{MF}$  and  $S_{C_2}$ .) As discussed earlier, methyl formate and  $C_2$  species were most likely formed from methoxy, formyl and formate species adsorbed on the Cu/metal oxide and that nucleophilic attack lead to methyl formate and  $C_2$  oxygenates. Subsequently, methyl formate was likely converted to  $\text{CH}_3\text{OH}$  and  $\text{CO}$  on  $\text{Cu}^0$ . Based on these observations and the correlation between intrinsic basicity and  $S_{MF}$ ,  $S_{C_2}$  and  $S_{CO}$ , it can be speculated that a balance of metal and basic sites are required for maximum selectivity to methyl formate and  $C_2$  oxygenates. At very high intrinsic basicities (the high loading K or Cs promoted Cu–MgO with intrinsic basicity >  $9.5 \mu\text{mol CO}_2 \text{ m}^{-2}$ ), although the formation of the methoxy species may be enhanced, the formyl and formate species would be reduced because of a reduced Cu surface area (Table 3). Note that Nunan et al. [14] also studied the effect of Cs loading on Cs–Cu–ZnO catalysts for methyl formate formation from syngas and concluded that there was an optimum Cs loading at which methyl formate yield reached a maximum value, in agreement with the present observations made regarding the effect of Cs loading on the Cs–Cu–MgO catalyst.

Hsiao and Lin [37] have studied the synthesis of methyl formate and higher alcohols over Cu–MgO– $\text{Al}_2\text{O}_3$  (Cu/MgO/ $\text{Al}_2\text{O}_3 = 4/5/91 \text{ wt}\%$ ) at 523 K, 101 kPa and  $W/F = 106.1 \times 10^{-3} \text{ min g}(\text{cm}^3(\text{STP})^{-1})$ . The study reported a total conversion of 82% with  $\text{CO}$ ,  $\text{CO}_2$  and  $\text{CH}_3\text{OCH}_3$  as the only products. The catalyst showed no activity towards methyl formate or  $C_2$  species, whereas over Cu–MgO in the present study, high selectivity towards methyl formate ( $S_{MF} = 29.3\%$ , Table 6) and low selectivity towards  $C_2$  species ( $S_{C_2} = 0.9\%$ , Table 6) was observed. The low Cu (4 wt%) and MgO (5 wt%) content of the Cu–MgO– $\text{Al}_2\text{O}_3$  catalyst used by Hsiao and Lin [37] and the presence of the acidic  $\text{Al}_2\text{O}_3$  support, results in the formation of  $\text{CH}_3\text{OCH}_3$ , generated by the acid catalysed dehydration of methanol. The  $S_{\text{BET}}$  and Cu dispersion for Cu–MgO– $\text{Al}_2\text{O}_3$  were reported as  $115 \text{ m}^2 \text{ g}^{-1}$  and 60%, respectively [37], whereas for the Cu–MgO of the present work, values of  $74 \text{ m}^2 \text{ g}^{-1}$  and 1.54%, respectively were obtained (Tables 2 and 3). These distinct differences, together with the higher temperature and  $W/F$  used by Hsiao and Lin [37] account for the differences in product distributions between the two studies.

## 5. Conclusion

High surface area MgO, Cu–MgO and alkali ( $\text{K}_2\text{O}$  and  $\text{Cs}_2\text{O}$ ) promoted Cu–MgO were prepared by thermal decomposition of metal salts in the presence of palmitic acid. The basicity of the catalysts decreased in the order: 13.5 wt% Cs–Cu–MgO > 4.4 wt% K–Cu–MgO > 0.5 wt% Cs–Cu–MgO > 0.5 wt% K–Cu–MgO > Cu–MgO > MgO. The intrinsic basicity of the Cu–MgO and alkali-promoted Cu–MgO catalysts were more than 10 times greater than a conventional Cu–ZnO catalyst. Over the alkali-promoted Cu–MgO catalysts at 101 kPa and 498 K with a  $\text{CO}/\text{He}/\text{CH}_3\text{OH}$  (0.20/0.66/0.14) feed gas, methyl formate was the primary product while  $\text{CO}$  was a secondary product.  $C_2$  species were also produced with low selectivity ( $S_{C_2} < 5\%$ ). Formation of methyl formate and  $C_2$  species were attributed to basic sites and  $\text{Cu}^0$  and there was an optimum basicity ( $9.5 \mu\text{mol CO}_2 \text{ m}^{-2}$ ) at which the  $S_{MF}$  and  $S_{C_2}$  reached a maximum.

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